

# *Nonlinear control of a zero stiffness magnetic spring*

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# *Here I am*

*What shall I talk about?*

Broadly speaking, two points:

1. Zero stiffness (and vibration isolation)
2. Nonlinear control

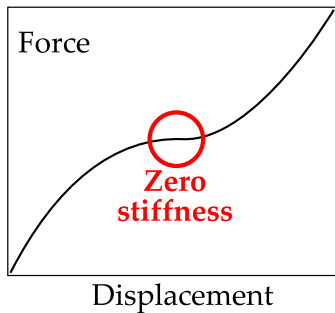
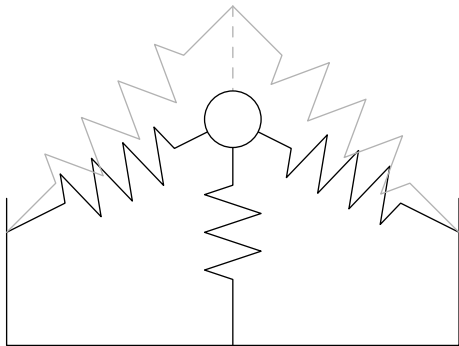
# What you say 'zero stiffness'?

Well, quasi-zero stiffness

1. Russian guys (1989)  
*'Vibration protecting and measuring systems with quasi-zero stiffness'*
2. Gert-Jan Nijssen (Twente, 2001)
3. Alex Carrella (ISVR, now)
4. Me (Adelaide, now)

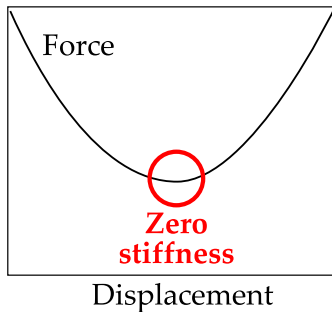
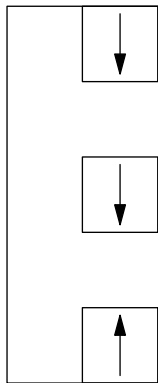
# Zero stiffness mechanisms

## Mechanical springs



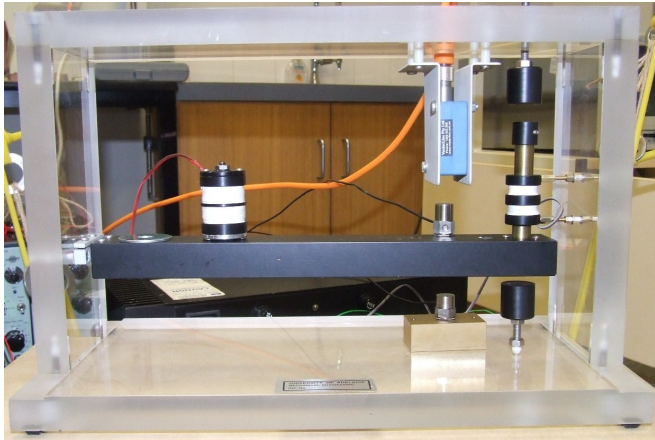
# Zero stiffness mechanisms

Unstable magnets



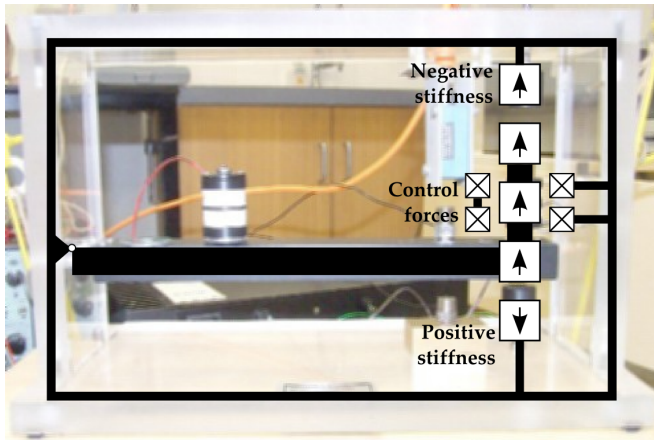
# Zero stiffness mechanisms

## Experimental rig

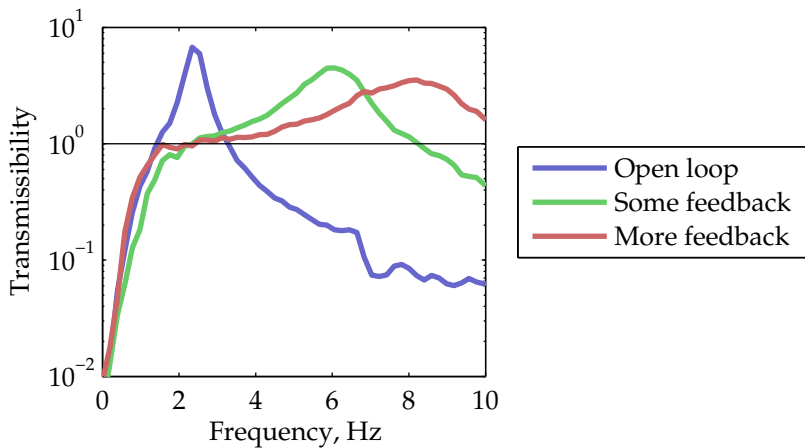


# Zero stiffness mechanisms

## Experimental rig



# Rig characteristics



## Nonlinear system model

A coupled mechanical-electrical system:

$$F_{\text{total}} = F_{\text{gravity}} + F_{\text{magnets}} + F_{\text{coil}} + F_{\text{damping}}$$

$$V_{\text{total}} = V_{\text{input}} + V_{\text{resistance}} + V_{\text{back-emf}}$$

That is:

$$M\ddot{x} = -Mg + F_{m_0} + K_m(x - x_0)^2 + K_c I - C_d \dot{x}$$

$$L\dot{I} = Gu - IR - K_c \dot{x}$$

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# Nonlinear control

*Krstic is my hero*

Backstepping controllers for 'lower triangular' systems such as: (albeit any number of states are possible)

$$\dot{x}_1 = x_2 + \varphi_1(x_1)^T \theta,$$

$$\dot{x}_2 = x_3 + \varphi_2(x_1, x_2)^T \theta,$$

$$\dot{x}_3 = u + \varphi_3(x_1, x_2, x_3)^T \theta,$$

with

- ▶ nonlinear  $\varphi_i$  known
- ▶ constant  $\theta$  unknown.

And there are classes of controllers for such systems...

# Nonlinear control

## Backstepping with tuning functions

$$z_1 = x_1 - y, \quad z_2 = x_2 - \alpha_1$$

$$z_3 = x_3 - \alpha_2, \quad u = \varrho_3 \alpha_3$$

$$\alpha_1 = -c_1 z_1$$

$$\alpha_3 = -\kappa_3 z_3 x_2^2 - \vartheta_5 x_2 + \partial_{x_1} \{\alpha_2\} x_2$$

$$- (x_1^4 + x_1^2$$

$$+ x_2^2 + x_3^2 + 1) \kappa_3 z_3 \partial_{x_2} \{\alpha_2\}^2$$

$$+ \partial_{\vartheta} \{\alpha_3\} \dot{\vartheta} - x_3 \vartheta_6 - \beta_2 z_2$$

$$- \kappa_3 z_2^2 z_3 - c_3 z_3 - x_3^2 \kappa_3 z_3$$

$$+ (\vartheta_1 + x_1 (\vartheta_2 + x_1 \vartheta_3))$$

$$+ x_2 \vartheta_4 + x_3 (\beta_2 + 2\kappa_3 z_2 z_3) \partial_{x_2} \{\alpha_2\}$$

$$+ \dot{\varrho}_2 \partial_{\varrho_2} \{\alpha_2\}$$

$$\alpha_2 = \varrho_2 (-\vartheta_3 x_1^2 - \vartheta_2 x_1 - x_1$$

$$+ y - \vartheta_1 - x_2 \vartheta_4 - c_2 z_2$$

$$- (x_1^4 + x_1^2 + x_2^2 + 1) \kappa_2 z_2$$

$$+ x_2 \partial_{x_1} \{\alpha_1\})$$

$$\dot{\vartheta} = \Gamma [z_2 - z_3 \partial_{x_2} \{\alpha_2\},$$

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$$x_2 z_3, x_3 z_3]^T,$$

$$\dot{\beta}_2 = -\gamma_2 z_3 (-x_2 + \alpha_1 + x_3 \partial_{x_2} \{\alpha_2\}),$$

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# Nonlinear control

*Mathematica to the rescue...*

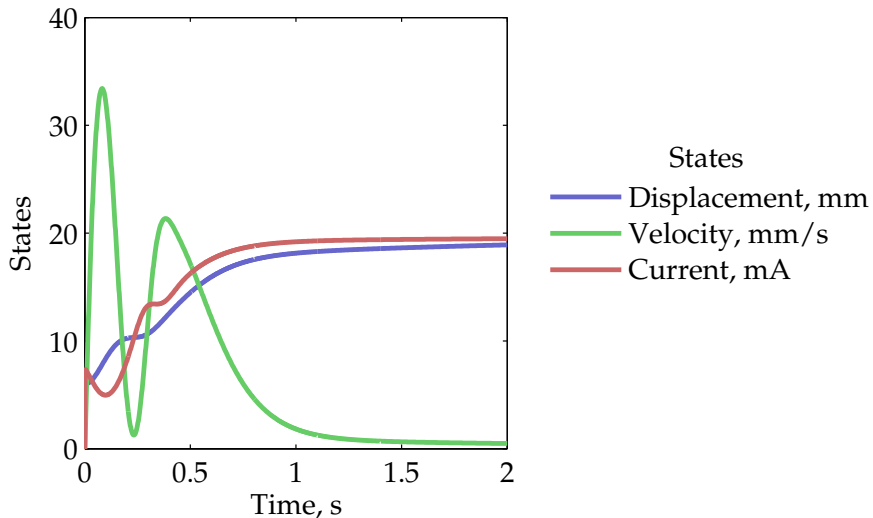
Mathematica is ideal for this task:

1. Control algebra calculated,
2. Embedded Matlab (or C) code written,
3. Output L<sup>A</sup>T<sub>E</sub>X typesetting code.

This is all *automatic*, and for a large class of nonlinear systems.

## But does it work?

Simulation results only at this stage...



# The end

1. Zero stiffness is a good idea for vibration isolation...
2. ...but impossible because it's unstable
3. Control can solve that problem...
4. ...but there's more work to be done

# Thanks

*It's been a great conference!*

- ▶ Email:  
`will@mecheng.adelaide.edu.au`
- ▶ Slides available at:  
`http://www.mecheng.adelaide.edu.au/~will/`